

# Linear stability analysis of viscous flow in axisymmetric domain

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## Abstract

The linear stability problem of an incompressible viscous flow between two concentric cylinders is investigated. Linearizing the transient behavior around a steady state solution leads to an eigenvalue problem for linearized Navier-Stokes equations. The discrete eigenvalue problem is obtained by the spectral element method. The algorithm is implemented in MATLAB. The developed program serves as a simple tool for numerical experimenting. The applicability of the program is validated through some few test computations.

## 1. Flow equations

Let  $D = \{(r, z) \mid r > 0\}$  is a 2D domain with the boundary  $\partial D \equiv \Gamma = \bar{\Gamma}_1 \cup \bar{\Gamma}_2$ ,  $\Gamma_1 \cap \Gamma_2 = \emptyset$ . Through the rotation of  $D$  about the  $z$ -axis we arrive at the axisymmetric 3D domain

$$V = \{(x, y, z) \mid x = r \cos \varphi, y = r \sin \varphi, (r, z) \in D, \varphi \in \langle 0, 2\pi \rangle\}$$

with the boundary  $\partial V \equiv S = \bar{S}_1 \cup \bar{S}_2$ ,  $S_1 \cap S_2 = \emptyset$ , where

$$S_i = \{(x, y, z) \mid x = r \cos \varphi, y = r \sin \varphi, (r, z) \in \Gamma_i, \varphi \in \langle 0, 2\pi \rangle\}, \quad i = 1, 2.$$

The Navier-Stokes equations in the cylindrical coordinate system  $(r, \varphi, z)$  rotating about the  $z$ -axis with angular velocity  $\Omega_0$  are (see e.g. [1])

$$\begin{aligned} \frac{\partial w_r}{\partial t} + w_r \frac{\partial w_r}{\partial r} + \frac{w_\varphi}{r} \frac{\partial w_r}{\partial \varphi} + w_z \frac{\partial w_r}{\partial z} - \frac{w_\varphi^2}{r} - 2\Omega_0 w_\varphi - \Omega_0^2 r &= \\ &= \frac{1}{\varrho} \left[ \frac{1}{r} \frac{\partial (r\tau_{rr})}{\partial r} + \frac{1}{r} \frac{\partial \tau_{r\varphi}}{\partial \varphi} + \frac{\partial \tau_{rz}}{\partial z} - \frac{\tau_{\varphi\varphi}}{r} \right], \end{aligned} \quad (1.1)$$

$$\begin{aligned} \frac{\partial w_\varphi}{\partial t} + w_r \frac{\partial w_\varphi}{\partial r} + \frac{w_\varphi}{r} \frac{\partial w_\varphi}{\partial \varphi} + w_z \frac{\partial w_\varphi}{\partial z} + \frac{w_r w_\varphi}{r} + 2\Omega_0 w_r &= \\ &= \frac{1}{\varrho} \left[ \frac{1}{r} \frac{\partial (r\tau_{\varphi r})}{\partial r} + \frac{1}{r} \frac{\partial \tau_{\varphi\varphi}}{\partial \varphi} + \frac{\partial \tau_{\varphi z}}{\partial z} + \frac{\tau_{\varphi r}}{r} \right], \end{aligned} \quad (1.2)$$

$$\frac{\partial w_z}{\partial t} + w_r \frac{\partial w_z}{\partial r} + \frac{w_\varphi}{r} \frac{\partial w_z}{\partial \varphi} + w_z \frac{\partial w_z}{\partial z} = \frac{1}{\varrho} \left[ \frac{1}{r} \frac{\partial (r\tau_{zr})}{\partial r} + \frac{1}{r} \frac{\partial \tau_{z\varphi}}{\partial \varphi} + \frac{\partial \tau_{zz}}{\partial z} \right]. \quad (1.3)$$

Here  $w_r$ ,  $w_\varphi$  and  $w_z$  are radial, circumferential and axial velocities,  $p$  is pressure,  $\varrho$  is density and  $\tau_{rr}$ ,  $\tau_{r\varphi}$ ,  $\tau_{rz}$ ,  $\tau_{\varphi r}$ ,  $\tau_{\varphi\varphi}$ ,  $\tau_{\varphi z}$ ,  $\tau_{zr}$ ,  $\tau_{z\varphi}$  and  $\tau_{zz}$  are stress tensor components,

$$\begin{aligned} \tau_{rr} &= -p + 2\mu \frac{\partial w_r}{\partial r}, & \tau_{r\varphi} &= \tau_{\varphi r} = \mu \left( \frac{1}{r} \frac{\partial w_r}{\partial \varphi} + \frac{\partial w_\varphi}{\partial r} - \frac{1}{r} w_\varphi \right), \\ \tau_{\varphi\varphi} &= -p + 2\mu \left( \frac{1}{r} \frac{\partial w_\varphi}{\partial \varphi} + \frac{1}{r} w_r \right), & \tau_{\varphi z} &= \tau_{z\varphi} = \mu \left( \frac{\partial w_\varphi}{\partial z} + \frac{1}{r} \frac{\partial w_z}{\partial \varphi} \right), \\ \tau_{zz} &= -p + 2\mu \frac{\partial w_z}{\partial z}, & \tau_{zr} &= \tau_{rz} = \mu \left( \frac{\partial w_z}{\partial r} + \frac{\partial w_r}{\partial z} \right), \end{aligned} \quad (1.4)$$

$\mu$  is dynamic viscosity.

Moreover, the velocities fulfill the continuity equation

$$\frac{1}{r} \frac{\partial (rw_r)}{\partial r} + \frac{1}{r} \frac{\partial w_\varphi}{\partial \varphi} + \frac{\partial w_z}{\partial z} = 0. \quad (1.5)$$

The Navier-Stokes equations and the continuity equation hold in the domain  $V$ . On the boundary  $S_1$  we prescribe velocities (essential boundary conditions)

$$w_r = \bar{w}_r, \quad w_\varphi = \bar{w}_\varphi, \quad w_z = \bar{w}_z \quad (1.6)$$

and on the boundary  $S_2$  we prescribe the stress vector components (natural boundary conditions)

$$\tau_{rr}n_r + \tau_{rz}n_z = \bar{p}_r, \quad \tau_{\varphi r}n_r + \tau_{\varphi z}n_z = \bar{p}_\varphi, \quad \tau_{zr}n_r + \tau_{zz}n_z = \bar{p}_z. \quad (1.7)$$

Here  $\mathbf{n} = (n_r, n_\varphi, n_z)$ ,  $n_\varphi = 0$ , is the unit outward normal vector to the boundary  $S_2$ . Bars in (1.6) and (1.7) denote known data.

## 2. The linear stability

Let us suppose that the steady base flow, whose stability we examine, is axially symmetric, described by functions

$$w_{0r}(r, z), \quad w_{0\varphi}(r, z), \quad w_{0z}(r, z), \quad p_0(r, z).$$

To investigate the stability of the base flow to disturbances, equations that govern the evolution of these perturbations are required. To this end, the base flow is perturbed by a disturbance velocity and pressure, i.e.

$$(w_r, w_\varphi, w_z, p) = (w_{0r}, w_{0\varphi}, w_{0z}, p_0) + \varepsilon(v_r, v_\varphi, v_z, \sigma), \quad (2.1)$$

and we examine, whether  $(w_r, w_\varphi, w_z, p) \rightarrow (w_{0r}, w_{0\varphi}, w_{0z}, p_0)$  for  $t \rightarrow \infty$ . Disturbances  $v_r, v_\varphi, v_z$  and  $\sigma$  depend on time  $t$  and on all three space variables  $r, \varphi$  and  $z$ , i.e.

$$v_r = v_r(t, r, \varphi, z), \quad v_\varphi = v_\varphi(t, r, \varphi, z), \quad v_z = v_z(t, r, \varphi, z), \quad \sigma = \sigma(t, r, \varphi, z).$$

If we substitute from (2.1) into equations (1.1)-(1.5), take into account the fact that the stationary flow functions  $w_{0r}, w_{0\varphi}, w_{0z}, p_0$  satisfy those equations and if we neglect terms containing  $\varepsilon^2$ , we obtain linearized Navier-Stokes equations

$$\begin{aligned} \frac{\partial v_r}{\partial t} + w_{0r} \frac{\partial v_r}{\partial r} + \frac{w_{0\varphi}}{r} \frac{\partial v_r}{\partial \varphi} + w_{0z} \frac{\partial v_r}{\partial z} + \frac{\partial w_{0r}}{\partial r} v_r + \frac{\partial w_{0r}}{\partial z} v_z - \frac{2}{r} w_{0\varphi} v_\varphi - 2\Omega_0 v_\varphi = \\ = \frac{1}{\varrho} \left[ \frac{1}{r} \frac{\partial (r\tau_{rr})}{\partial r} + \frac{1}{r} \frac{\partial \tau_{r\varphi}}{\partial \varphi} + \frac{\partial \tau_{rz}}{\partial z} - \frac{\tau_{\varphi\varphi}}{r} \right], \end{aligned} \quad (2.2)$$

$$\begin{aligned} \frac{\partial v_\varphi}{\partial t} + w_{0r} \frac{\partial v_\varphi}{\partial r} + \frac{w_{0\varphi}}{r} \frac{\partial v_\varphi}{\partial \varphi} + w_{0z} \frac{\partial v_\varphi}{\partial z} + \frac{\partial w_{0\varphi}}{\partial r} v_r + \frac{\partial w_{0\varphi}}{\partial z} v_z + \frac{w_{0r}}{r} v_\varphi + \frac{w_{0\varphi}}{r} v_r + 2\Omega_0 v_r = \\ = \frac{1}{\varrho} \left[ \frac{1}{r} \frac{\partial (r\tau_{\varphi r})}{\partial r} + \frac{1}{r} \frac{\partial \tau_{\varphi\varphi}}{\partial \varphi} + \frac{\partial \tau_{\varphi z}}{\partial z} + \frac{\tau_{\varphi r}}{r} \right], \end{aligned} \quad (2.3)$$

$$\begin{aligned} \frac{\partial v_z}{\partial t} + w_{0r} \frac{\partial v_z}{\partial r} + \frac{w_{0\varphi}}{r} \frac{\partial v_z}{\partial \varphi} + w_{0z} \frac{\partial v_z}{\partial z} + \frac{\partial w_{0z}}{\partial r} v_r + \frac{\partial w_{0z}}{\partial z} v_z = \\ = \frac{1}{\varrho} \left[ \frac{1}{r} \frac{\partial (r\tau_{zr})}{\partial r} + \frac{1}{r} \frac{\partial \tau_{z\varphi}}{\partial \varphi} + \frac{\partial \tau_{zz}}{\partial z} \right]. \end{aligned} \quad (2.4)$$

Stresses in (2.2)-(2.4) have the form (1.4), where we replace  $p$  by  $\sigma$  and  $w$  by  $v$ . The continuity equation reads

$$\frac{1}{r} \frac{\partial (rv_r)}{\partial r} + \frac{1}{r} \frac{\partial v_\varphi}{\partial \varphi} + \frac{\partial v_z}{\partial z} = 0. \quad (2.5)$$

Velocities  $v_r, v_\varphi, v_z$  and pressure  $\sigma$  fulfill homogeneous boundary conditions

$$v_r = v_\varphi = v_z = 0 \quad \text{on } S_1, \quad (2.6)$$

$$\tau_{rr}n_r + \tau_{rz}n_z = 0, \quad \tau_{\varphi r}n_r + \tau_{\varphi z}n_z = 0, \quad \tau_{zr}n_r + \tau_{zz}n_z = 0 \quad \text{on } S_2. \quad (2.7)$$

The stability problem, therefore, consists in verifying whether

$$(v_r, v_\varphi, v_z, \sigma) \rightarrow (0, 0, 0, 0) \quad \text{pro } t \rightarrow \infty. \quad (2.8)$$

### 3. The eigenvalue problem

Let  $I = \sqrt{-1}$  is the imaginary unit and  $n$  is a natural number. Using the transformation

$$(v_r, v_\varphi, v_z, \sigma) = e^{\lambda t + In\varphi} (u_r, u_\varphi, u_z, h), \quad (3.1)$$

where  $u_r, u_\varphi, u_z$  and  $h$  are functions of the two variables  $r, z$  and  $\lambda$  is a complex number, we separate out the time  $t$  as well as the azimuthal coordinate  $\varphi$ . For  $n = 0$  we obtain the rotationally symmetric flow. We insert (3.1) into (2.2)-(2.5), remove the term  $e^{\lambda t + In\varphi}$  and obtain the eigenvalue problem in the  $(r, z)$ -plane ( $\lambda$  is an eigenvalue and  $\mathbf{u} := (u_r, u_\varphi, u_z, h)$  is an eigenfunction)

$$\begin{aligned} \lambda u_r + w_{0r} \frac{\partial u_r}{\partial r} + \frac{nI}{r} w_{0\varphi} u_r + w_{0z} \frac{\partial u_r}{\partial z} + \frac{\partial w_{0r}}{\partial r} u_r + \frac{\partial w_{0r}}{\partial z} u_z - \\ - \frac{2}{r} w_{0\varphi} u_\varphi - 2\Omega_0 u_\varphi = \frac{1}{\varrho} \left[ \frac{1}{r} \frac{\partial (r\tau_{rr})}{\partial r} + \frac{nI}{r} \tau_{r\varphi} + \frac{\partial \tau_{rz}}{\partial z} - \frac{\tau_{\varphi\varphi}}{r} \right], \end{aligned} \quad (3.2)$$

$$\begin{aligned} \lambda u_\varphi + w_{0r} \frac{\partial u_\varphi}{\partial r} + \frac{nI}{r} w_{0\varphi} u_\varphi + w_{0z} \frac{\partial u_\varphi}{\partial z} + \frac{\partial w_{0\varphi}}{\partial r} u_r + \frac{\partial w_{0\varphi}}{\partial z} u_z + \\ + \frac{w_{0r}}{r} u_\varphi + \frac{w_{0\varphi}}{r} u_r + 2\Omega_0 u_r = \frac{1}{\varrho} \left[ \frac{1}{r} \frac{\partial (r\tau_{\varphi r})}{\partial r} + \frac{nI}{r} \tau_{\varphi\varphi} + \frac{\partial \tau_{\varphi z}}{\partial z} + \frac{\tau_{\varphi r}}{r} \right], \end{aligned} \quad (3.3)$$

$$\begin{aligned} \lambda u_z + w_{0r} \frac{\partial u_z}{\partial r} + \frac{nI}{r} w_{0\varphi} u_z + w_{0z} \frac{\partial u_z}{\partial z} + \frac{\partial w_{0z}}{\partial r} u_r + \frac{\partial w_{0z}}{\partial z} u_z = \\ = \frac{1}{\varrho} \left[ \frac{1}{r} \frac{\partial (r\tau_{zr})}{\partial r} + \frac{nI}{r} \tau_{z\varphi} + \frac{\partial \tau_{zz}}{\partial z} \right], \end{aligned} \quad (3.4)$$

$$\frac{1}{r} \frac{\partial (ru_r)}{\partial r} + \frac{1}{r} \frac{\partial u_\varphi}{\partial \varphi} + \frac{\partial u_z}{\partial z} = 0. \quad (3.5)$$

The stress components now are

$$\begin{aligned} \tau_{rr} &= -h + 2\mu \frac{\partial u_r}{\partial r}, & \tau_{r\varphi} &= \tau_{\varphi r} = \mu \left( \frac{nI}{r} u_r + \frac{\partial u_\varphi}{\partial r} - \frac{1}{r} u_\varphi \right), \\ \tau_{\varphi\varphi} &= -h + 2\mu \left( \frac{nI}{r} u_\varphi + \frac{1}{r} u_r \right), & \tau_{\varphi z} &= \tau_{z\varphi} = \mu \left( \frac{\partial u_\varphi}{\partial z} + \frac{nI}{r} u_z \right), \\ \tau_{zz} &= -h + 2\mu \frac{\partial u_z}{\partial z}, & \tau_{zr} &= \tau_{rz} = \mu \left( \frac{\partial u_z}{\partial r} + \frac{\partial u_r}{\partial z} \right). \end{aligned} \quad (3.6)$$

Further, we derive the variational formulation. Let  $\psi_r, \psi_\varphi, \psi_z$  and  $q$  are test functions of the two variables  $r$  and  $z$  and let

$$\psi_r = \psi_\varphi = \psi_z = 0 \quad \text{on } \Gamma_1. \quad (3.7)$$

We multiply the equation (3.2) by  $r\psi_r$ , the equation (3.3) by  $r\psi_\varphi$ , the equation (3.4) by  $r\psi_z$ , the equation (3.5) by  $rq$ , integrate over  $D$  and apply the Green theorem (with

respect to terms containing stresses  $\tau_{rr}, \tau_{rz}, \tau_{\varphi r}, \tau_{\varphi z}, \tau_{zr}, \tau_{zz}$ ). If we take into account (2.7) and (3.7), we obtain

$$\int_D \left\{ \left[ \lambda u_r + w_{0r} \frac{\partial u_r}{\partial r} + \frac{nI}{r} w_{0\varphi} u_r + w_{0z} \frac{\partial u_r}{\partial z} + \frac{\partial w_{0r}}{\partial r} u_r + \frac{\partial w_{0r}}{\partial z} u_z - \frac{2}{r} w_{0\varphi} u_\varphi - 2\Omega_0 u_\varphi \right] \psi_r + \frac{1}{\varrho} \left[ \tau_{rr} \frac{\partial \psi_r}{\partial r} - \frac{nI}{r} \tau_{r\varphi} \psi_r + \tau_{rz} \frac{\partial \psi_r}{\partial z} + \frac{\tau_{\varphi\varphi}}{r} \psi_r \right] \right\} r \, dr \, dz = 0, \quad (3.8)$$

$$\int_D \left\{ \left[ \lambda u_\varphi + w_{0r} \frac{\partial u_\varphi}{\partial r} + \frac{nI}{r} w_{0\varphi} u_\varphi + w_{0z} \frac{\partial u_\varphi}{\partial z} + \frac{\partial w_{0\varphi}}{\partial r} u_r + \frac{\partial w_{0\varphi}}{\partial z} u_z + \frac{w_{0r}}{r} u_\varphi + \frac{w_{0\varphi}}{r} u_r + 2\Omega_0 u_r \right] \psi_\varphi + \frac{1}{\varrho} \left[ \tau_{\varphi r} \frac{\partial \psi_\varphi}{\partial r} - \frac{nI}{r} \tau_{\varphi\varphi} \psi_\varphi + \tau_{\varphi z} \frac{\partial \psi_\varphi}{\partial z} - \frac{\tau_{r\varphi}}{r} \psi_\varphi \right] \right\} r \, dr \, dz = 0, \quad (3.9)$$

$$\int_D \left\{ \left[ \lambda u_z + w_{0r} \frac{\partial u_z}{\partial r} + \frac{nI}{r} w_{0\varphi} u_z + w_{0z} \frac{\partial u_z}{\partial z} + \frac{\partial w_{0z}}{\partial r} u_r + \frac{\partial w_{0z}}{\partial z} u_z \right] \psi_z + \frac{1}{\varrho} \left[ \tau_{zr} \frac{\partial \psi_z}{\partial r} - \frac{nI}{r} \tau_{z\varphi} \psi_z + \tau_{zz} \frac{\partial \psi_z}{\partial z} \right] \right\} r \, dr \, dz = 0, \quad (3.10)$$

$$\int_D \left\{ \frac{\partial u_r}{\partial r} + \frac{nI}{r} u_\varphi + \frac{\partial u_z}{\partial z} + \frac{u_r}{r} q \right\} r \, dr \, dz = 0. \quad (3.11)$$

Moreover, we add essential boundary conditions

$$u_r = u_\varphi = u_z = 0 \quad \text{on } \Gamma_1. \quad (3.12)$$

The stability expressed by the relation (2.8) occurs if all eigenvalues  $\lambda$  of the problem (3.8) - (3.12) have negative real parts.

## 4. The discretization

The approximate finite-dimensional eigenvalue problem is obtained by the spectral element method. The algorithm was implemented in MATLAB. The generalized eigenvalue problem

$$\mathbf{A}u = \lambda \mathbf{B}u \quad (4.1)$$

was solved by means of MATLAB function `eig`. In what follows we describe the intimated process more detaily.

The spectral element method is a discretization technique, which has excellently approved as a solution method for incompressible flows problems, see e.g. [2], [3], [8], [6]. We decided to use this method mainly because the spectral element approximation of the eigenvalue problem promise to be sufficiently representative already at a low order of

matrices  $\mathbf{A}$  and  $\mathbf{B}$ , as theory as well as a practise indicate. Let us show in brief how an approximate eigenvalue problem can be obtained.

We restrict ourselves to the case that  $D$  is a rectangle,

$$D = \{(r, z) \mid 0 < R_1 < r < R_2, 0 < z < L\}. \quad (4.2)$$

We divide  $D$  into  $n_r \times n_z$  concurrent rectangular elements  $D^{ij}$ ,  $i = 1, 2, \dots, n_r$ ,  $j = 1, 2, \dots, n_z$ , with sides of length  $d_r = (R_2 - R_1)/n_r$  and  $d_z = L/n_z$  in the direction of the  $r$ -axis and  $z$ -axis, respectively. The corresponding partition of the interval  $\langle R_1, R_2 \rangle$  and  $\langle 0, L \rangle$  is determined by points

$$r_i = R_1 + id_r, \quad i = 0, 1, \dots, n_r, \quad z_j = jd_z, \quad j = 0, 1, \dots, n_z.$$

The element  $D^{ij}$  is the image of the reference element  $\hat{D} = (-1, 1)^2$  under the transformation

$$r^{ij}(\xi) = R_1 + [i - 1 + \frac{1}{2}(\xi + 1)] d_r, \quad z^{ij}(\eta) = [j - 1 + \frac{1}{2}(\eta + 1)] d_z, \quad [\xi, \eta] \in \hat{D}. \quad (4.3)$$

If

$$-1 = \xi_0 < \xi_1 < \dots < \xi_{N-1} < \xi_N = 1$$

are nodes of the Gauss-Legendre-Lobatto quadrature formula (briefly GLL formula) of order  $2N - 1$ , see e.g. [2], then images  $[r_k^{ij}, z_\ell^{ij}]$  of nodes  $[\xi_k, \xi_\ell]$  under the transformation (4.3),

$$r_k^{ij} = r^{ij}(\xi_k), \quad z_\ell^{ij} = z^{ij}(\xi_\ell), \quad k, \ell = 0, 1, \dots, N,$$

are nodes of the product GLL quadrature formula on the element  $D^{ij}$ .

We approximate velocities  $u_r$ ,  $u_\varphi$  and  $u_z$  with piecewise polynomial functions  $u_{r,\vartheta}$ ,  $u_{\varphi,\vartheta}$  and  $u_{z,\vartheta}$ , which are on every element  $D^{ij}$  interpolation polynomials  $u_{r,\vartheta}^{ij}$ ,  $u_{\varphi,\vartheta}^{ij}$  and  $u_{z,\vartheta}^{ij}$  of degree  $N$  uniquely determined by their values  $u_{r,k\ell}^{ij}$ ,  $u_{\varphi,k\ell}^{ij}$ ,  $u_{z,k\ell}^{ij}$  at the nodes  $[r_k^{ij}, z_\ell^{ij}]_{k,\ell=0}^N$ . The lower index  $\vartheta$  specifies the quality of the approximation:  $\vartheta = (d, N)$ , where  $d = \max(d_r, d_z)$  represents the fineness of partition and  $N$  is the degree of polynomial approximation.

Similarly, we introduce nodes  $[\tilde{r}_k^{ij}, \tilde{z}_\ell^{ij}]$  of the product Gauss-Legendre quadrature formula (briefly GL formula) on the element  $D^{ij}$ ,

$$\tilde{r}_k^{ij} = r^{ij}(\tilde{\xi}_k), \quad \tilde{z}_\ell^{ij} = z^{ij}(\tilde{\xi}_\ell), \quad k, \ell = 1, \dots, N - 1,$$

where

$$-1 < \tilde{\xi}_1 < \tilde{\xi}_2 < \dots < \tilde{\xi}_{N-2} < \tilde{\xi}_{N-1} < 1$$

are nodes of the GL formula of order  $2N - 3$ , see e.g. [2]. We approximate pressure  $h$  with piecewise polynomial function  $h_{\tilde{\vartheta}}$ , which is on every element  $D^{ij}$  an interpolation polynomial  $h_{\tilde{\vartheta}}^{ij}$  of degree  $N - 2$  uniquely determined by its values  $\tilde{h}_{k\ell}^{ij}$  at nodes  $[\tilde{r}_k^{ij}, \tilde{z}_\ell^{ij}]_{k,\ell=1}^{N-1}$ , where  $\tilde{\vartheta} = (d, N - 2)$ .

The fulfillment of boundary conditions can be achieved by zeroing interpolants at nodes lying on  $\bar{\Gamma}_1$ .

Further, we replace stationary velocities  $w_{0r}$ ,  $w_{0\varphi}$  and  $w_{0z}$  by their interpolations  $u_{0r,\vartheta}$ ,  $u_{0\varphi,\vartheta}$  and  $u_{0z,\vartheta}$ , which are again piecewise polynomials of degree  $N$ , whose values  $w_{0r,kl}^{ij}$ ,  $w_{0\varphi,kl}^{ij}$  and  $w_{0z,kl}^{ij}$  at nodes  $[r_k^{ij}, z_\ell^{ij}]$  are supposed to be known.

We also replace test functions  $\psi_r$ ,  $\psi_\varphi$ ,  $\psi_z$  by their interpolants  $\psi_{r,\vartheta}$ ,  $\psi_{\varphi,\vartheta}$ ,  $\psi_{z,\vartheta}$  (which are piecewise polynomials of degree  $N$ , on  $D^{ij}$  determined by their values  $\psi_{r,kl}^{ij}$ ,  $\psi_{\varphi,kl}^{ij}$ ,  $\psi_{z,kl}^{ij}$  at nodes  $[r_k^{ij}, z_\ell^{ij}]$ ) and  $q$  by the interpolant  $q_\vartheta$  (which is a piecewise polynomial of degree  $N - 2$ , on  $D^{ij}$  determined by its values  $\tilde{q}_{k\ell}^{ij}$  at nodes  $[\tilde{r}_k^{ij}, \tilde{z}_\ell^{ij}]$ ). Test functions  $\psi_{r,\vartheta}$ ,  $\psi_{\varphi,\vartheta}$ ,  $\psi_{z,\vartheta}$  equal to zero in GLL nodes lying on the boundary  $\bar{\Gamma}_1$ .

We insert all interpolants into equations (3.8)-(3.11) and (3.6), express integrals over the whole domain  $D$  as a sum of integrals over individual elements  $D^{ij}$  and every from those integrals compute numerically: integrals containing pressure  $h_{\tilde{\vartheta}}$  or test function  $q_{\tilde{\vartheta}}$  with the GL formula and remaining integrals with the GLL formula.

We rearrange the matrix  $\{u_{r,kl}^{ij}\}_{k,\ell=0}^N$  of parameters determining the function  $u_{r,\vartheta}^{ij}$  into the column vector

$$\mathbf{u}_r^{ij} = (u_{r,00}^{ij}, u_{r,10}^{ij}, \dots, u_{r,N0}^{ij}, u_{r,01}^{ij}, u_{r,11}^{ij}, \dots, u_{r,N1}^{ij}, \dots, u_{r,0N}^{ij}, u_{r,1N}^{ij}, \dots, u_{r,NN}^{ij})^T.$$

Vectors of parameters  $\mathbf{u}_\varphi^{ij}$ ,  $\mathbf{u}_z^{ij}$  and  $\tilde{\mathbf{h}}^{ij}$  will be obtained similarly. We merge all unknown parameters into one column vector  $\mathbf{u}^{ij}$ ,

$$[\mathbf{u}^{ij}]^T = ([\mathbf{u}_r^{ij}]^T, [\mathbf{u}_\varphi^{ij}]^T, [\mathbf{u}_z^{ij}]^T, [\tilde{\mathbf{h}}^{ij}]^T)^T.$$

If

$$[\boldsymbol{\psi}^{ij}]^T = ([\boldsymbol{\psi}_r^{ij}]^T, [\boldsymbol{\psi}_\varphi^{ij}]^T, [\boldsymbol{\psi}_z^{ij}]^T, [\mathbf{q}^{ij}]^T)^T$$

is the corresponding vector of test functions parameters, then summing all approximate equations we arrive at the equation

$$\sum_{i=1}^{n_r} \sum_{j=1}^{n_z} [\boldsymbol{\psi}^{ij}]^T (\lambda \mathbf{B}^{ij} - \mathbf{A}^{ij}) \mathbf{u}^{ij} = 0.$$

Arranging all nonzero components of vectors  $\mathbf{u}^{ij}$  and  $\boldsymbol{\psi}^{ij}$  into column vectors  $\mathbf{u}$  and  $\boldsymbol{\psi}$  enables to write the preceding equation in the form

$$\boldsymbol{\psi}^T (\lambda \mathbf{B} - \mathbf{A}) \mathbf{u} = 0,$$

and as the vector  $\boldsymbol{\psi}$  is arbitrary, we obtain the generalized eigenvalue problem (4.1).

The matrix  $\mathbf{A}$  is regular, nonhermitian, real for  $n = 0$  and complex for  $n > 0$ . The matrix  $\mathbf{B}$  is diagonal and singular: diagonal coefficients corresponding to parameters  $\mathbf{q}^{ij}$  are equal to zero, remaining diagonal coefficients are real and positive.

## 5. Numerical examples

We choose the data having regard to the following technical problem. Water enter the pipe through the boundary  $\Gamma_{in} = \bar{D} \cap \{z = 0\}$  and leaves it through the boundary  $\Gamma_{out} = \bar{D} \cap \{z = L\}$ .  $\Gamma_{wall} = \bar{D} \cap \{r = R_2\}$  is the wall of the pipe and  $\Gamma_{rope} = \bar{D} \cap \{r = R_1\}$  is the interface between water and the cavitating vapour rope. In this case we have

$$\begin{aligned}\Gamma_1 &= \Gamma_{in} \cup \Gamma_{wall} = \{(r, z) \in \Gamma \mid z = 0 \text{ or } r = R_2\}, \\ \Gamma_2 &= \Gamma_{out} \cup \Gamma_{rope} = \{(r, z) \in \Gamma \mid z = L \text{ or } r = R_1\}.\end{aligned}\tag{5.1}$$

Further, we chose  $R_1 = 0.015$ ,  $R_2 = 0.15$ ,  $L = 0.5$  and  $\varrho = 10^3$ . Dynamical viscosity of water  $\mu = 10^{-3}$ , but we will experiment also with another values of  $\mu$ .

*Example 1.* We consider a hypothetical flow as a solid body movement. We take  $w_{0r} = 0$ ,  $w_{0\varphi} = 0$ ,  $w_{0z} = C_0$ , use the boundary partition (5.1) and experiment with values of  $C_0 \geq 0$ ,  $\Omega_0$ ,  $\mu$ ,  $n$ ,  $n_r$ ,  $n_z$  and  $N$ . The flow of this type is stable and numerical computations confirm this. With  $\mu = 0$  we have the inviscid flow, corresponding numerical results were published in [5] (for  $\mu = 0$  we have only the condition  $u_r = 0$  on  $\Gamma_{wall}$ ). When  $\mu$  increases, then  $\max \text{Re}(\lambda)$  increases as well, i.e. the stability grows. In the table 1 we introduce typical results.

$\mu$	$10^{-3}$	$10^{-2}$	$10^{-1}$	1	$10^1$	$10^2$	$10^3$
$\max \text{Re}(\lambda)$	-0.30	-0.36	-0.84	-3.78	-11.30	-70.10	-665.26

Table 1: The stability increase,  $n = 0$ ,  $C_0 = \Omega_0 = 1$ ,  $n_r = n_z = 1$ ,  $N = 8$ .

*Example 2.* We consider the flow between two concentric rotating cylinders. By  $\Omega_1$  and  $\Omega_2$  we denote the angular velocity of the inner and outer cylinder, respectively. Then

$$w_{0r} = w_{0z} = 0, \quad w_{0\varphi} = \frac{(R_2^2 \Omega_2 - R_1^2 \Omega_1) r^2 + R_1^2 R_2^2 (\Omega_1 - \Omega_2)}{(R_2^2 - R_1^2) r},\tag{5.2}$$

see e.g. [7]. The stability of this flow is known as the Taylor-Couette problem.

(a) If we consider an inviscid flow, i.e.  $\mu = 0$ , then the classical Taylor's result claims: the flow is stable if and only if

$$\frac{\Omega_2}{\Omega_1} > \frac{R_1^2}{R_2^2},\tag{5.3}$$

see e.g. [7]. Numerical computations confirm this theoretical result. We take

$$\Gamma_1 = \bar{D} \cap (\{z = 0\} \cup \{r = R_1\} \cup \{r = R_2\}), \quad \Gamma_2 = \bar{D} \cap \{z = L\}\tag{5.4}$$

and set  $\Omega_1 = 1$ . Then the stability should arise for

$$\Omega_2 > \frac{0.015^2}{0.15^2} = 0.01.$$



We take  $n = 0$ ,  $N = 4$ ,  $n_z = 1$  and find that the lowest value of  $\Omega_2$ , for which the program gives nonnegative real parts of all eigenvalues, converge to 0.01 if  $n_r$  increases, see Table 2 (values of  $\min \Omega_2$  are rounded to 4 decimal places).

$n_r$	1	2	4	8	16	32
$\min \Omega_2$	0.0418	0.0328	0.0200	0.0126	0.0104	0.0100

Table 2: The lowest attainable angular velocity  $\Omega_2$ ,  $n_z = 1$ ,  $N = 4$ .

(b) In case of viscous flows the stability significantly increases. We carried out the following numerical experiment: for  $\mu = 1$ ,  $n = 0$ ,  $n_r = n_z = 1$ ,  $N = 8$  and the boundary partition (5.4) we took several values of  $\Omega_2$  and for each of them we found the critical value  $\Omega_{1,crit}(\Omega_2)$ , where the onset of instability occurs (i.e.  $\Omega_{1,crit}(\Omega_2)$  is the point of transition from the stable to unstable flow regime for a given  $\Omega_2$ ). Results in the  $(\Omega_2, \Omega_1)$ -phase plane are presented in Figure 1. We have found that for  $\Omega_1 < 43$  the Couette flow remains stable for all values of  $\Omega_2$ . The dotted line denotes the stability border for  $\mu = 0$ . Our numerical results qualitatively agree with well known Taylor's experimental results, see e.g. [7].

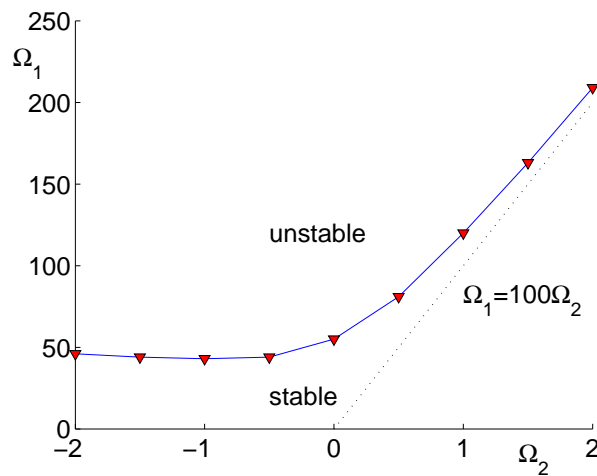


Figure 1: The stability of Couette flow.

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