

# On the two-scale finite element method for the heat transfer in buildings

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The design of modern engineered buildings cannot avoid understanding non-stationary thermal behaviour of buildings, its prediction and modification. of the design of modern engineered buildings. Reliable mathematical models and corresponding software codes should contain information about a (quasi)periodic material microstructure. One possible approach is to apply the correction algorithm for (not necessarily conforming) two-scale finite element discretization (Glowinski et al. 2004) to a special parabolic problem (using the sequences of Rothe) and to combine it with the two-scale homogenization theory (Nguetseng 1989, Allaire 1992, Holmbom 1995, Cioranescu & Donato 1999, etc.).

Let  $\Omega$  be a domain in  $R^3$ ,  $V = W^{1,2}(\Omega)$  and  $I = [0, T]$  (a time interval). The most simple technically realistic problem of heat transfer is to find such temperature  $\tau \in L^2(I, V)$  with a time derivative  $\dot{\tau} \in L^2(I, V^*)$  that, in terms of scalar products  $(\cdot, \cdot)$  in  $L^2(\Omega)$  and  $\langle \cdot, \cdot \rangle$  in  $L^2(\partial\Omega)$ ,

$$(v, \tilde{c}\dot{\tau}) + (\nabla v, \tilde{a}\nabla\tau) + \langle v, b\tau \rangle = \langle v, b\tau^\times \rangle \quad \forall v \in V;$$

some additional assumptions related to material characteristics  $a, b, c$  are needed,  $\sim$  refers to some “effective values” (rarely known a priori), the temperature of outer environment  $\tau^\times$  and initial values of  $\tau$  in zero time are prescribed. The discretized forms for two (macro- and micro-) scales are

$$(v_h, \tilde{c}(\tau_{sh} - \tau_{s-1h}))/H + (\nabla v_h, \tilde{a}\nabla\tau_{sh}) + \langle v_h, b\tau_{sh} \rangle = \langle v_h, b\tau_{sh}^\times \rangle \quad \forall v_h \in V_h,$$

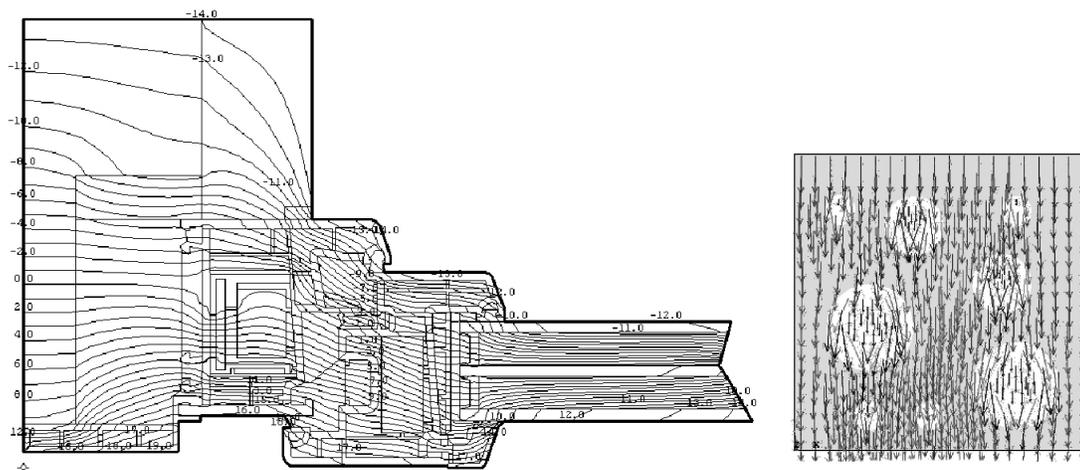
$$(v_\delta, c(\cdot/\varepsilon)(\tau_{s\delta}^\varepsilon - \tau_{s-1\delta}^\varepsilon))/H + (\nabla v_\delta, a(\cdot/\varepsilon)\nabla\tau_{s\delta}^\varepsilon) + \langle v_\delta, b\tau_{s\delta}^\varepsilon \rangle = \langle v_\delta, b\tau_{s\delta}^\times \rangle \quad \forall v_\delta \in V_\delta$$

where  $h, H, \delta \rightarrow 0$ ,  $h \gg \delta$ ,  $V_h$  and  $V_\delta$  are finite-dimensional subspaces of  $V$ ,  $s \in \{1, 2, \dots, T/H\}$ ,  $\varepsilon$  is a characteristic microstructural size ( $\varepsilon \rightarrow 0$  during homogenization) and  $a, c$  are periodic on certain parallelepipeds in  $R^3$ . The convergence properties of a special iterative process can be compared with classical finite element techniques.

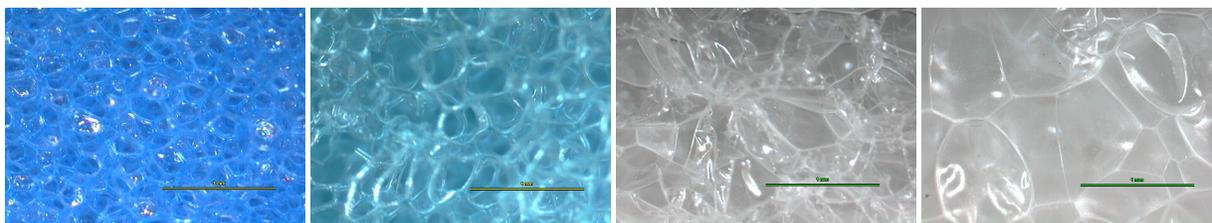
The full version CD-ROM version of this paper includes:

1. overview of modelling of the heat transfer in buildings,
2. analysis of two-scale grids and two-scale homogenization,
3. description of an iterative computational algorithm for the stationary heat transfer.

Two upper illustrative figures show i) temperature isotherms in a part of certain advanced (macroscopic) window construction, ii) distributions of heat fluxes  $-A\nabla\tau$  in a non-homogenous rubber-based insulation layer in great detail (a square with edge length 0.1 mm). Our original stationary problem in  $R^3$  is reduced to the two-dimensional one, all computations are ANSYS-supported.



The lower sequence of figures demonstrates some typical examples of microstructure of real insulation materials.



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